



# Anti-parity-time symmetry enabled on-chip chiral polarizer

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Encircling an exceptional point (EP) in a parity-time (PT) symmetric system has shown great potential for chiral optical devices, such as chiral mode switching for symmetric and antisymmetric modes. However, to our best knowledge, chiral switching for polarization states has never been reported, although chiral polarization manipulation has significant applications in imaging, sensing, communication, etc. Here, inspired by the anti-PT symmetry, we demonstrate, for the first time to our best knowledge, an on-chip chiral polarizer by constructing a polarization-coupled anti-PT symmetric system. The transmission axes of the chiral polarizer are different for forward and backward propagation. A polarization extinction ratio of over 10 dB is achieved for both propagating directions. Moreover, a telecommunication experiment is performed to demonstrate the potential applications in polarization encoding signals. It provides a novel functionality for encircling-an-EP parametric evolution and offers a new approach for on-chip chiral polarization manipulation. © 2021 Chinese Laser Press

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## 1. INTRODUCTION

Non-Hermitian systems, especially parity-time (PT) symmetric systems, have attracted widespread attention for their fascinating physical properties and broad applications. Fruitful advances have been achieved in the field of PT symmetry [1], such as unidirectional propagation and lasing [2–8], single-mode lasing [9–12], sense enhancement [13–18], and optoelectronics oscillators [19,20]. Notably, owing to the non-Hermiticity-induced nonadiabatic transitions, chiral mode switching was achieved for symmetric and antisymmetric modes by encircling the exceptional point (EP) in a PT symmetric system [21–29], exhibiting great potential for chiral devices [7,27,30]. However, different from the spatial modes, it is unsuitable to perform the encircling EP evolution in an on-chip PT symmetric system for chiral polarization switching, because the polarization modes are asymmetrical, and the coupling between two orthogonal polarization states needs not only the match of effective indexes of the two polarization modes but also the share of a common parallel polarization component between them. As a result, the chiral polarization switching to date has not been yielded. However, as a basic property of light, polarization has abundant applications, such as communication

[31–33], imaging [34–36], and storage [37]. Thus, chiral polarization switching can inspire fascinating interest into handling polarization information.

As the counterpart of PT symmetric systems, anti-PT symmetric systems were first proposed by Ge and Türeci in 2013 [38], conjugated to those observed in PT-symmetric ones [39]. Many novel phenomena about anti-PT symmetry have been observed, e.g., sensing enhancement [40], coherent perfect absorption lasing [41], heat transfer [42], topological superconductors [43], and chiral dynamics [44]. Different from the PT symmetry, the eigenmodes of anti-PT symmetric systems are asymmetrical when the real parts of the corresponding eigenvalue split, which exactly matches the polarization mode characteristics. Anti-PT symmetry shows great potential in physics and applications. For practical optical applications, anti-PT symmetry has harsh requirements of pure imaginary coupling coefficients, which were demonstrated by indirectly dissipative coupling [45], nonlinear coupling [46], spinning the resonator [47], etc. Benefiting from these breakthroughs, anti-PT symmetry can be heralded as a powerful tool to design optical devices with fascinating properties. Notably, the indirect coupling in anti-PT symmetric systems makes it possible to construct chiral polarization switching.

In this paper, we propose and experimentally demonstrate a chiral polarizer based on an anti-PT symmetric system for the first time. Conventional polarizers operate by rejecting undesired polarization, and the transmission axes are the same for bidirectional propagation, whereas, our chiral polarizer operates by rotating the orthogonal polarization state to the transmission axis [48] and exhibits different transmission axes for forward and backward propagation. We induce a transitional mode between transverse electric (TE) and transverse magnetic (TM) modes and realize the encircling-an-EP parametric evolution in an integrated polarization-coupled anti-PT symmetric system. For arbitrary input polarization states, we achieve a polarization extinction ratio of 10 dB between the transmission of TE and TM modes over a bandwidth from 1550 to 1590 nm. Moreover, the application of polarization data formatting is also demonstrated by a communication experiment with a bit rate of 10 Gbit/s on-off keying signals. Our work demonstrates a practicable application for encircling EP in non-Hermitian systems and provides a novel tool for future polarization manipulating such as data formatting and polarization-multiplexing duplex communication.

## 2. RESULT

### A. Principle of Chiral Polarization Switching

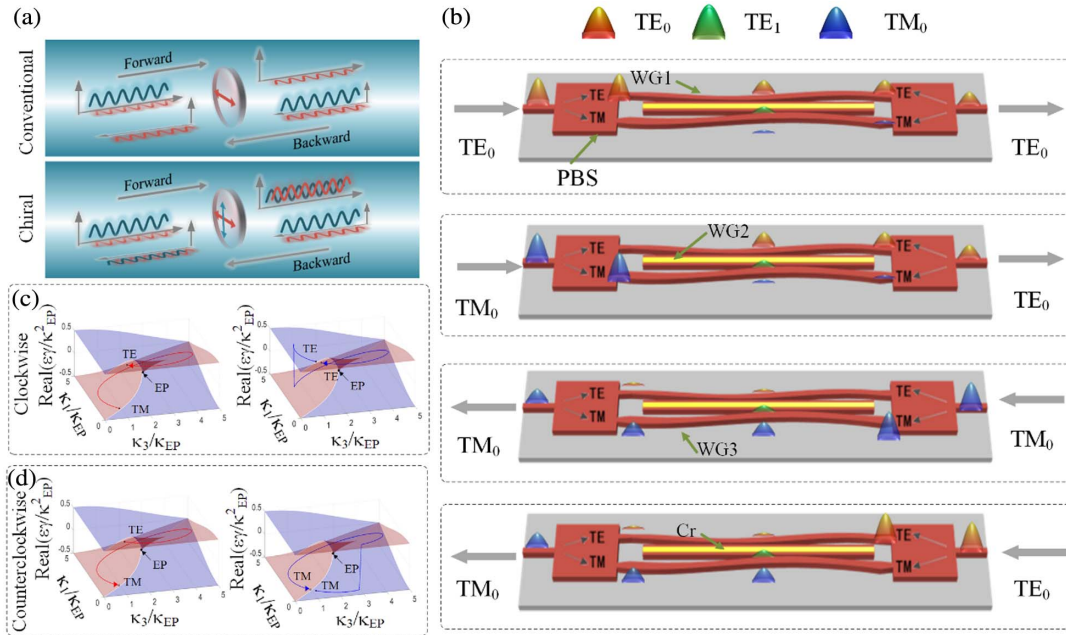
Figure 1(a) shows the comparison between a conventional polarizer and our chiral polarizer. The chiral polarizer exhibits different transmission axes for forward and backward propagation. In forward propagation, the output polarization state will be rotated to the vertical direction no matter what the input polarization states are. However, in backward propagation, the output polarization state will be rotated to the horizontal direction. This chiral dynamic can be used for on-chip

polarization data formatting or polarization multiplexing duplex operation. It should be noted that a conventional polarizer operates by rejecting undesired polarization, and the transmission axes are the same for bidirectional propagation. Figure 1(b) illustrates the chip structure of the chiral polarizer, constructed with a three-waveguide coupled region and two polarization beam splitters (PBSs). The three-waveguide coupled region consists of three waveguides, WG1, WG2, and WG3, where WG1 and WG3 support TE<sub>0</sub> and TM<sub>0</sub> modes, respectively, and WG2 supports the transitional TE<sub>1</sub> mode. The coupled region is a dual-port system, in which the TE<sub>0</sub> and TM<sub>0</sub> modes are processed separately. When light is injected from the left, the output mode is TE<sub>0</sub> regardless of TE<sub>0</sub> or TM<sub>0</sub> injection, whereas, when light is injected from the right, the output mode is TM<sub>0</sub> for both TE<sub>0</sub> and TM<sub>0</sub> injection. The PBS is used to decompose the input light into TE<sub>0</sub> and TM<sub>0</sub> modes and combine the output light to handle arbitrary polarization. The anti-PT symmetry is realized by the indirect dissipate coupling between WG1 and WG3. We use the coupled-mode theory to analyze the system. The model Hamiltonian takes the form

$$H = \begin{bmatrix} \beta_1 & \kappa_1 & 0 \\ \kappa_1 & \beta_2 + i\gamma & \kappa_3 \\ 0 & \kappa_3 & \beta_3 \end{bmatrix}, \quad (1)$$

where  $\gamma$  is the loss of WG2, which can be tuned by introducing a chromium (Cr) strip on top of WG2;  $\beta_1$ ,  $\beta_2$ , and  $\beta_3$  are the propagation constants of modes in WG1, WG2, and WG3, respectively.  $\kappa_1$  is the coupling coefficient between WG1 and WG2, and  $\kappa_3$  is that between WG2 and WG3. The eigenvalue is given by

$$\lambda = \frac{\beta_1 + \beta_3}{2} + i\frac{\kappa_1\kappa_3}{\gamma} \pm i\sqrt{\frac{\kappa_1^2\kappa_3^2}{\gamma^2} - \left(\frac{\beta_1 - \beta_3}{2} + i\frac{\kappa_1^2 - \kappa_3^2}{2\gamma}\right)^2}$$



**Fig. 1.** Concept and scheme of the chiral polarizer. (a) Comparison between conventional polarizer and our chiral polarizer. (b) Scheme of our chiral polarizer. The chiral polarizer is constructed with three waveguides WG1, WG2, and WG3; where WG1 and WG3 are supposed to be lossless, and WG2 has a high loss. (c) Encircling EP evolution clockwise. (d) Encircling EP evolution counterclockwise.

with an assumption of  $|\gamma| \gg |\lambda - \beta_2|$ . The detailed analysis is described in Appendix A. The normalized complex-eigenvalue spectra

$$\varepsilon = \pm i \frac{\kappa_{\text{EP}}^2}{\gamma} \sqrt{\frac{\kappa_1^2 \kappa_3^2}{\kappa_{\text{EP}}^4} - \left[ \text{sign}(\beta_1 - \beta_3) + i \frac{\kappa_1^2 - \kappa_3^2}{2\kappa_{\text{EP}}^2} \right]^2}$$

dependent on  $\kappa_1/\kappa_{\text{EP}}$  and  $\kappa_3/\kappa_{\text{EP}}$  form a Riemann surface, as shown in Figs. 1(c) and 1(d), where the EP point can be specified by  $\kappa_1^2 = \kappa_3^2 = \gamma(\beta_1 - \beta_3)/2 = \kappa_{\text{EP}}^2$ . The encircling-EP evolution can be acquired by suitably changing  $\kappa_1$  and  $\kappa_3$  along the propagation direction. In that case, chiral polarization switching can be achieved because of the non-Hermiticity-induced nonadiabatic transitions [49]. Due to the presence of absorption, the self-intersecting Riemann surface is separated into gain surface (red) and loss surface (blue). Each point on the surface represents an eigenvalue of the system. By changing the system parameters, the eigenvalue can move on the surface. The path can form a ring around the EP if the parameters are well managed, that is, the encircling EP evolution. The nonadiabatic hopping occurs only when the eigenvalue is moving on the loss surface, which leads to the different final states for encircling the EP clockwise and counterclockwise. Inspired by this chiral dynamic, it is possible to apply encircling EP evolution to guide the design of chiral polarizer.

Figure 1(c) shows the process of the eigenvalue moving clockwise on the Riemann surface. In this direction, the  $\text{TE}_0$  mode moves on the loss surface. Due to the presence of absorption, the evolution of  $\text{TE}_0$  mode cannot maintain on the loss surface for the entire loop and hops to the gain surface during the evolution. As a result, the  $\text{TE}_0$  mode returns to itself without mode flipping. However, the  $\text{TM}_0$  mode moves on the gain surface, which indicates that the evolution of the  $\text{TM}_0$  mode can survive to the end without hopping and complete the mode flipping. Figure 1(d) demonstrates the evolution in counterclockwise direction. In contrast with the process in the clockwise direction, the  $\text{TM}_0$  mode moves on the loss surface, while the  $\text{TE}_0$  mode moves on the gain surface when encircling EP in the counterclockwise direction. Figures 1(c) and 1(d) indicate that the final polarization state of light for encircling EP clockwise is the  $\text{TE}_0$  mode and that for encircling EP counterclockwise is the  $\text{TM}_0$  mode, no matter the state of original polarization.

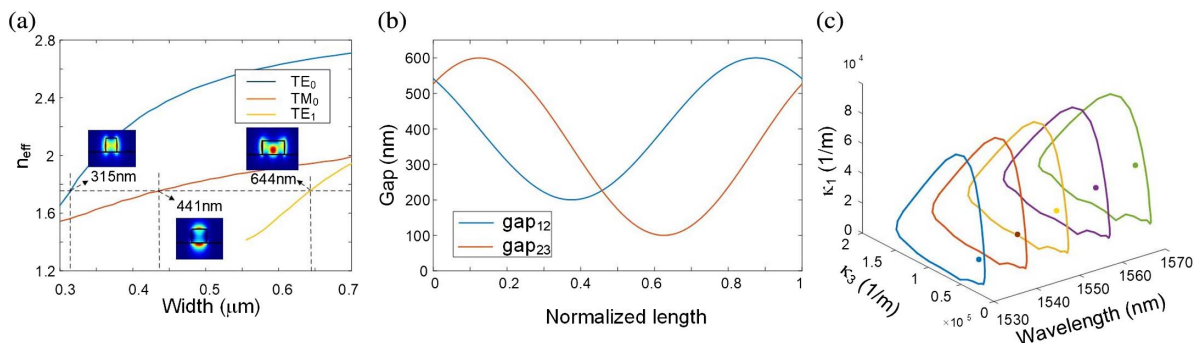
## B. Design of the Chiral Polarizer

Figure 2 shows the design details of the proposed chiral polarizer. The device is designed on a silicon-on-insulator (SOI) platform with 250 nm top silicon and 2  $\mu\text{m}$  buried oxide. We use the finite difference time domain method to calculate the mode field distribution and effective refractive index of each mode in waveguides with different widths, as shown in Fig. 2(a). In order to realize mode coupling, the effective refractive indexes of the three modes in respective waveguides must be approximately equal. On this premise, the widths of the waveguides are designed to be 315 nm for WG1, 441 nm for WG3, and 644 nm for WG2, which are marked by the dashed lines in Fig. 2(a). A Cr strip with a width of 100 nm and a thickness of 100 nm is deposited on the top of WG2 to induce the absorption loss ( $\gamma$ ).

The coupling coefficients  $\kappa_1$  and  $\kappa_3$  can be controlled by changing the gaps between waveguides. Figure 2(b) shows the gap variation along the propagation direction between WG1 and WG2 ( $\text{gap}_{12}$ ) and that between WG2 and WG3 ( $\text{gap}_{23}$ ), which are given by

$$\begin{aligned} \text{gap}_{12} &= \frac{\text{gap}_0}{2} + 100 \text{ nm} - \left( \frac{\text{gap}_0}{2} - 100 \text{ nm} \right) \times \cos\left(\frac{z}{L} - \frac{3}{4}\pi\right), \\ \text{gap}_{23} &= \frac{\text{gap}_0}{2} + 50 \text{ nm} - \left( \frac{\text{gap}_0}{2} - 50 \text{ nm} \right) \times \sin\left(\frac{z}{L} - \frac{3}{4}\pi\right), \end{aligned} \quad (2)$$

where  $z$  is the propagation distance,  $L$  is the total length of the coupled region, and  $\text{gap}_0 = 600$  nm is the maximum gap between the two waveguides. As the propagation distance of  $z$  increases from 0 to  $L$ , the parametric variation gives rise to a closed curve in the  $(\kappa_1, \kappa_3)$  plane. Figure 2(c) shows the closed loops around EPs at different wavelengths. EPs at different wavelengths are marked by the points in Fig. 2(c). The loops clearly encircle the EPs over a spectrum range from 1530 to 1570 nm, which covers the C-band for optical communication. It should be noted that an arbitrary polarization state can be decomposed into  $x$  and  $y$  polarization components with a particular amplitude ratio and phase difference. As a result, the input light with an arbitrary polarization state is first split into  $\text{TE}_0$  and  $\text{TM}_0$  modes by a PBS in our device and then starts the encircling EP evolution. The  $\text{TE}_0$  and  $\text{TM}_0$  modes enter the coupled region through WG1 and WG3, respectively, after PBS. The length of the coupling region is 110  $\mu\text{m}$ ,



**Fig. 2.** Detailed design of chiral polarizer. (a) Effective refractive index of each mode versus the width of waveguide. (b) Optimized gap transform function that generates encircling EP parametric evolution. (c) Wavelength-dependent parametric loops for the design shown in (a) and (b).

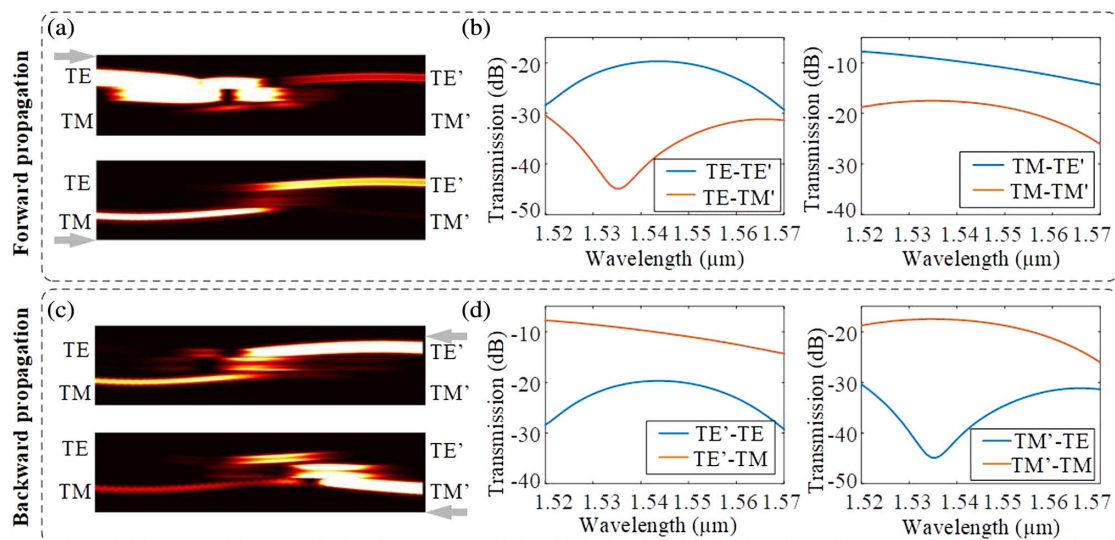
corresponding to the  $L$  in Eq. (2). A longer coupling region will lead to a higher extinct ratio but a higher loss. A  $110\ \mu\text{m}$  coupling length is a good trade-off between the extinction ratio and loss. Figure 3(a) shows the field distributions of  $\text{TE}_0$  and  $\text{TM}_0$  modes excited from different directions at  $1540\ \text{nm}$ . It can be seen clearly that  $\text{TE}_0$  and  $\text{TM}_0$  modes are both transmitted to the  $\text{TE}_0$  mode and output from WG1 when the light is injected from the left ports (i.e., forward propagation), whereas, they are both transmitted to the  $\text{TM}_0$  mode and output from WG3 when the light is injected from the right ports (i.e., backward propagation). The corresponding transmission spectra are shown in Fig. 3(b), which indicate that the chiral dynamics occurs over a spectrum range from  $1520$  to  $1570\ \text{nm}$ . A  $10\ \text{dB}$  extinction ratio is also accomplished from  $1530$  to  $1560\ \text{nm}$ , which can be used for the chiral polarizer.

### C. Fabrication and Experiment

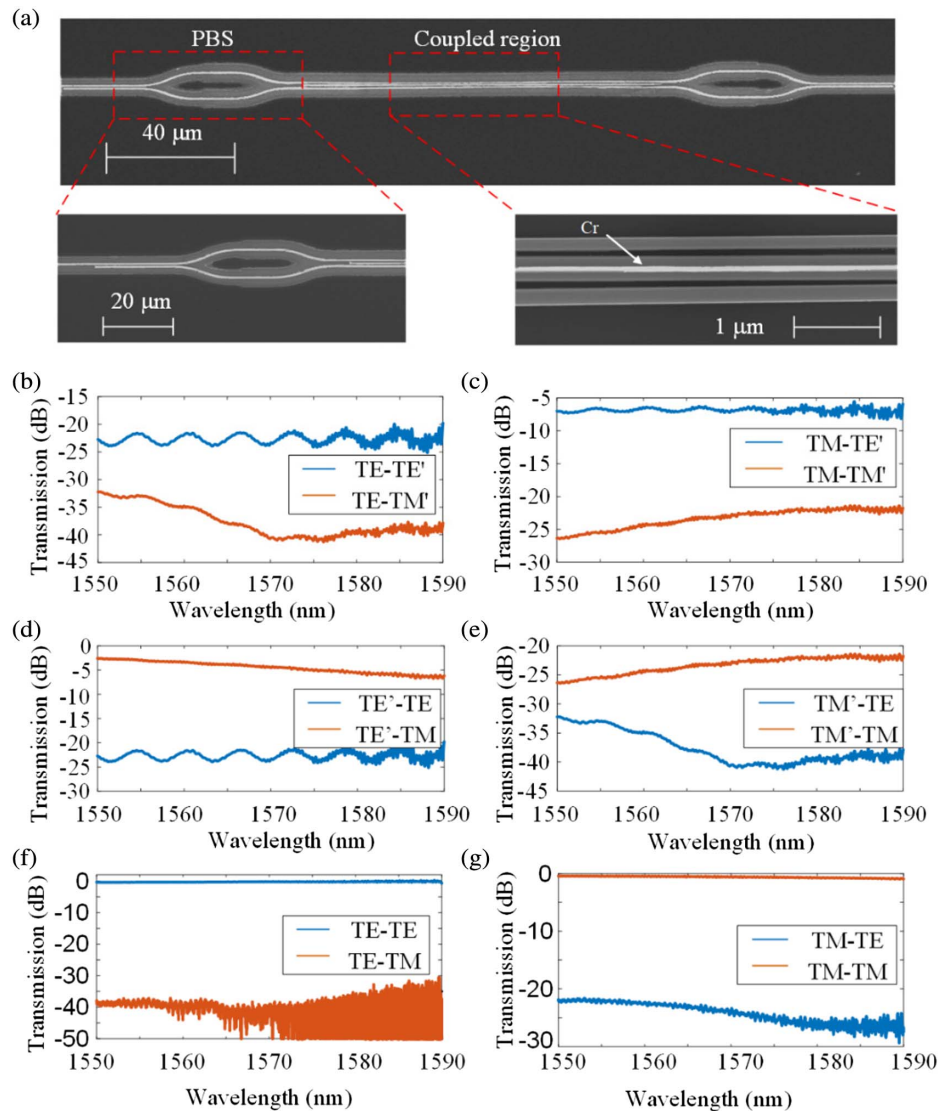
The device is fabricated by a standard electron-beam (e-beam) lithography-based nanofabrication process on the commercial  $250\ \text{nm}$  SOI platform. The scanning electron microscope (SEM) is used to determine the dimensions of the devices and confirm the obtained geometric shape, as shown in Fig. 4(a). The detailed structures of PBS and coupling region are presented as insets in Fig. 4(a) with the tested spectrum shown in Figs. 4(f) and 4(g); the fabrication of PBS is presented in the Appendix B [50]. The device is characterized by measuring the transmission spectra. The measured transmission spectra for  $\text{TE}_0$  and  $\text{TM}_0$  injection are shown in Figs. 4(b)–4(e). TE and TM denote the input or output mode from the left, and TE' and TM' denote the input or output mode from the right. Figures 4(b) and 4(c) demonstrate the output spectra for forward propagation. It can be seen clearly that the  $\text{TE}_0$  is the dominant output mode whichever  $\text{TE}_0$  or  $\text{TM}_0$  mode is inputted, whereas the  $\text{TM}_0$  mode becomes the dominant output mode for backward propagation, as shown in Figs. 4(d) and 4(e). The oscillations of the experimental spectra are due to the resonances between the facets of the coupling

fiber. A  $10\ \text{dB}$  extinction ratio is achieved from  $1550$  to  $1590\ \text{nm}$ . The polarizer exhibits a loss of  $\sim 25\ \text{dB}$  for  $\text{TE}_0$  input from the left and  $\text{TM}_0$  input from the right. This loss is the intrinsic property of encircling EP in a passive system, which can be reduced by shortening the coupling length. It is a trade-off between insertion loss and extinction ratio. For more practical applications, the coupling length should be designed carefully or induce gain to balance the loss. Compared with the simulation results, the experiment spectra are redshifted, which is mainly caused by fabrication errors. According to Fig. 2(a), the refractive indexes dependent on waveguide width in  $\text{TE}_0$  and  $\text{TE}_1$  modes have high slopes, which indicate that the fabrication errors may manifest a vital impact on the performance of device. In fact, we have tested different devices with gradually varied parameters. The asymmetric mode switching phenomenon can be observed when the deviation of the widths of waveguides is lower than  $10\ \text{nm}$ . The insertion loss is mainly influenced by the width of the Cr strip. A wider Cr strip leads to higher insertion loss. For a well-performed device, the fabrication error should be controlled within  $\sim 10\ \text{nm}$ .

To further verify the practical communication performances of the proposed chiral polarizer, a communication experiment is demonstrated to perform a function of formatting the data encoded on polarization channels into a particular polarization state. The experiment setup is illustrated in Fig. 5(a). The on-off keying (OOK) data are encoded on the  $\text{TE}_0$  and  $\text{TM}_0$  modes, where the  $\text{TE}_0$  mode indicates “1” and  $\text{TM}_0$  mode indicates “0.” Without loss of generality, the polarization encoded signals can be decomposed into data loaded on the  $\text{TE}_0$  mode and its inverted data loaded on the  $\text{TM}_0$  mode. In the experiment, the  $10\ \text{GHz}$  random OOK data and its inverted data are generated by an arbitrary waveform generator and loaded on the  $\text{TE}_0$  and  $\text{TM}_0$  modes by intensity modulator (IM), respectively. An erbium-doped fiber amplifier is used to compensate the power difference between  $\text{TE}_0$  and  $\text{TM}_0$  modes induced by the chiral polarizer. Data streams loaded on  $\text{TE}_0$  and  $\text{TM}_0$  modes are combined by the PBS and injected into the chip.



**Fig. 3.** Simulation results of the chiral polarizer. (a) Simulation power distributions in the waveguides for forward and backward propagation. (b) Transmission spectra for different input.

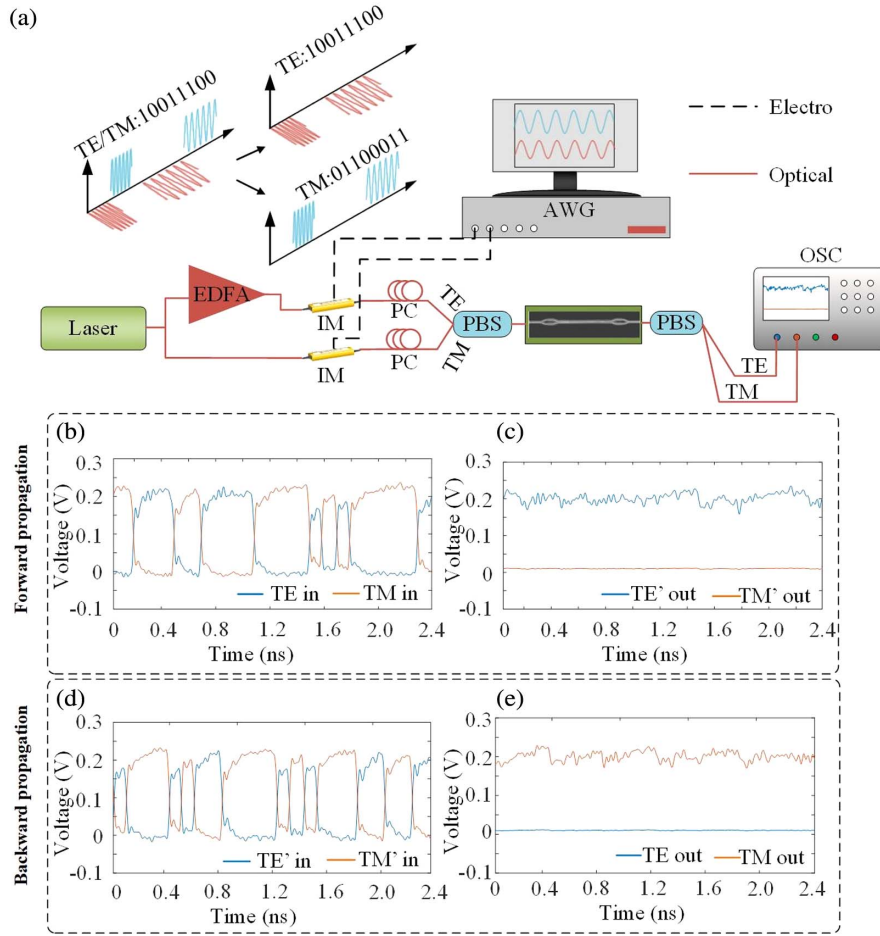


**Fig. 4.** SEM images of the chip and the experimentally measured spectra. (a) SEM images of the proposed chiral polarizer. Zoom-in images of polarization beam splitter and coupled region are shown in the subgraphs. (b)–(e) Experimentally measured spectra of the device for the (b), (c) forward propagation and (d), (e) backward propagation. TE and TM denote the modes input or output from the left; TE' and TM' denote the modes input or output from the right. (f), (g) Test results of the PBS.

The output light is decomposed into  $TE_0$  and  $TM_0$  modes and received by the oscilloscope. The input waveforms for forward and backward propagation is shown in Figs. 5(b) and 5(d), respectively. The output  $TE_0$  and  $TM_0$  polarization components of light are shown in Figs. 5(c) and 5(e). According to the analysis above, the data stream loaded on different polarization states transporting forward will be formatted into the  $TE_0$  mode. It can be seen clearly in Fig. 5(c) that most signal power is transferred to the  $TE_0$  mode, while only a little signal power remains in the  $TM_0$  mode. However, the  $TM_0$  mode becomes the dominant mode when the data transports backward. Figure 5(e) shows that most signal power transferred to  $TM_0$  mode rather than  $TE_0$  mode, which indicates the function of polarization data formatting with our chiral polarizer. An extinction ratio of 13 and 14 dB for forward and backward propagation is achieved, respectively.

### 3. CONCLUSION

In summary, we have proposed a chiral polarizer in an anti-PT symmetric system, which forms different polarized states dependent on light propagation direction. Based on the indirect coupling property of the anti-PT symmetric system, we successfully build an on-chip polarization-coupled anti-PT symmetric system for the first time. With the encircling EP evolution, we implement the chiral asymmetry polarization switch and chiral polarizer. The proposed chiral polarizer has been successfully applied to polarization data formatting for polarization encoding signals. The extinction ratio between the  $TE_0$  and  $TM_0$  modes for forward and backward propagation is 13 and 14 dB, respectively. Our work provides a new on-chip polarization manipulation method and demonstrates a practicable application in optics for encircling EP in non-Hermitian systems.



**Fig. 5.** Experiment setup and results of communication experiment. (a) Experiment setup. (b) The 10 GHz OOK bits stream loaded on TE and TM modes for inputting forward. (c) Power summary of the output TE and TM modes. (d), (e) Result of inputting backward. TE and TM denote the input or output modes from the left; TE' and TM' denote the input or output modes from the right.

## APPENDIX A: THEORY OF INDIRECT DISSIPATED COUPLING OF ANTI-PT SYMMETRIC SYSTEM

For the three-waveguide-coupled system shown in Fig. 1(b), WG1 and WG3 are supposed to be lossless, and WG2 has a high loss. In this case, the complex amplitudes in these waveguides satisfy the mode coupling equation, given by

$$\begin{bmatrix} \beta_1 & \kappa_1 & 0 \\ \kappa_1 & \beta_2 + i\gamma & \kappa_3 \\ 0 & \kappa_3 & \beta_3 \end{bmatrix} \begin{bmatrix} E_1 \\ E_2 \\ E_3 \end{bmatrix} = \lambda \begin{bmatrix} E_1 \\ E_2 \\ E_3 \end{bmatrix}, \quad (\text{A1})$$

where  $E$  is the complex amplitude of each mode and  $\beta$  is the propagation coefficient.  $\kappa_1$  is the coupling coefficient between WG1 and WG2, while  $\kappa_3$  is the coupling coefficient between WG2 and WG3. By substituting  $E_1$  and  $E_3$  for  $E_2$ , and, under the assumption of  $|\gamma| \gg |\lambda - \beta_2|$ , Eq. (A1) can be simplified as

$$\begin{bmatrix} \beta_1 + \frac{i\kappa_1^2}{\gamma} & \frac{i\kappa_1\kappa_3}{\gamma} \\ \frac{i\kappa_1\kappa_3}{\gamma} & \beta_3 + \frac{i\kappa_3^2}{\gamma} \end{bmatrix} \begin{bmatrix} E_1 \\ E_3 \end{bmatrix} = \lambda \begin{bmatrix} E_1 \\ E_3 \end{bmatrix}. \quad (\text{A2})$$

The eigenvalue of this degenerate second-order system can be written as

$$\lambda = \frac{\beta_1 + \beta_3}{2} + i \frac{\kappa_1\kappa_3}{\gamma} \pm i \sqrt{\frac{\kappa_1^2\kappa_3^2}{\gamma^2} - \left( \frac{\beta_1 - \beta_3}{2} + i \frac{\kappa_1^2 - \kappa_3^2}{2\gamma} \right)^2}. \quad (\text{A3})$$

Equation (A3) indicates that the system has an EP at  $\kappa_1^2 = \kappa_3^2 = \gamma |\frac{\beta_1 - \beta_3}{2}|$ . Encircling EP evolution can be obtained by changing  $\kappa_1$  and  $\kappa_3$  along the propagation direction.

In Eq. (A3), we suppose  $\kappa_1 = \kappa_3$ ,  $\Delta = \frac{\beta_1 - \beta_3}{2}$ , and  $\Omega^2 = \frac{\kappa_1^2\kappa_3^2}{\gamma^2} - (\frac{\beta_1 - \beta_3}{2})^2$ . When  $\Omega^2 > 0$ , the imaginary part of the eigenvalue splits, and the eigenvector can be written as  $E_{1,3} = [1, (\pm|\Omega| + i\Delta) \frac{\gamma}{\kappa_1\kappa_3}]^T$ . The phase differences between two complex amplitudes in WG1 and WG3 are close to 0 and  $\pi$ , indicating that the symmetry of the system is unbroken. When  $\Omega^2 < 0$ , the real part of the eigenvalue splits, and the eigenvector of the system can be written as  $E_{1,3} = [1, i(\Delta \mp |\Omega|) \frac{\gamma}{\kappa_1\kappa_3}]^T$ . The phase differences between two complex amplitudes in WG1 and WG3 are  $\frac{\pi}{2}$ , indicating that the symmetry of the system is broken. Compared with the PT symmetric system, an anti-PT symmetric system shows the opposite degenerate condition of real and imaginary parts of the

eigenvalue in broken and unbroken states. This property indicates that the indirect coupling in the three-waveguide-coupled system can be used to construct the anti-PT symmetric system, which lays the foundation of our work.

## APPENDIX B: FABRICATION AND TEST RESULT OF ON-CHIP PBS

We use on-chip PBSs to split the input light into TE and TM modes and recombine the output light. The PBS is based on a directional coupler, which has a significantly larger  $TM_0$  coupling coefficient than the  $TE_0$  mode coupling coefficient. The coupling length is selected so that the  $TM_0$  mode achieves full coupling, while the  $TE_0$  mode remains negligible coupling. The PBS is fabricated by electron beam lithography (EBL) and inductively coupled plasma (ICP) etching. The insertion loss of the PBS for TE input is negligible and for TM input is about 1 dB; further, the extinction ratio is tested by TE and TM mode input, respectively. The extinction ratio is 35 dB for the TE mode input. For the TM mode input, the extinction ratio is 23 dB. The light splitting ability of PBS is enough for our chiral polarizer.

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**Data Availability.** Additional data related to this paper are available from the corresponding author upon request.

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